

# DETERMINATION OF THE THERMAL EXPANSION COEFFICIENT FOR A NEW TYPE ALLOY STEEL

Veselin TSONEV

Technical University of Sofia, Bulgaria

**Abstract.** The subject of research in the present paper is the experimental determination of the thermal expansion coefficient for a definite type of steel at high temperatures. The presented methodology is proved by investigation of a new type of steel.

**Keywords:** thermal expansion, steel, residual stress

## 1. Introduction

Computer simulations significantly contribute to the improvement of mould technologies. That is why they are widely used in practice. Specialized commercial software is usually utilized. There are not many software products which offer options for calculation of residual stress and strain and their capabilities to adapt to specific problems are not always sufficient. A lot of studies are made by using universal software products in which calculation models are created [1].

Simulation of residual stresses and strains at moulding requires accurate information about the properties of the used materials. Some of these properties can be obtained from specialized literature or from experimental data. Some of the material properties are temperature-dependent and they have different degree of influence over the results from a numerical solution. Significant experience is required to decide which properties should be accurately determined (by experimental investigation) and which can be taken with an approximate value from literature resources when defining a numerical model.

A temperature change  $\Delta t$  of a structural element leads to a change of its length  $L$  which can be expressed by  $\Delta L' = \alpha \cdot \Delta t \cdot L$ , where  $\alpha$  is the material thermal expansion coefficient for the relevant temperature range [2]. In the case of a mould the uneven cooling induces residual stresses [3]. Important parameter in a numerical simulation of such stresses in moulds is the material thermal expansion coefficient. Determination of the elongation which a specimen made of definite material undertakes at 1°C temperature change can lead to obtaining of this coefficient.

## 2. Aim of the study

The study aims to obtain the thermal expansion coefficient of a new type alloy steel 1.4852 M

developed by Centromet PLC – Vratsa. The chemical ingredients of the alloy steel are given in Table 1. The steel is used for mould production.

Table 1. Chemical composition of steel 1.4852 M (in %)

C	0.45÷0.5
Ni	45÷48
Cr	34÷37
Si	≤2.2
Mn	≤1.5
Nb	≤1.8
S	≤0.03
P	≤0.03
Ti	0.1÷0.25
Zr	0.1÷0.2

## 3. Experimental study and results

The specimens made of the investigated steel are shown in Figure 1. They are made according to the standard EN 10291:2000 [5].



Figure 1. Test pieces

The experiments are conducted with a testing stand which is shown in Figure 2. It consists of heating device, testing machine and equipment for control and recording of experimental data [4]. The heating device allows the test specimens to be heated to 1100 °C.

The extensometer used for the longitudinal deformations measurement is shown in Figure 3. It is produced by Epsilontech (USA). Its range is up to 1100°C and the initial measurement length is 25 mm. The extensometer corresponds to the standard EN 10002-4 [6].



Figure 2. A stand for testing materials at elevated temperatures

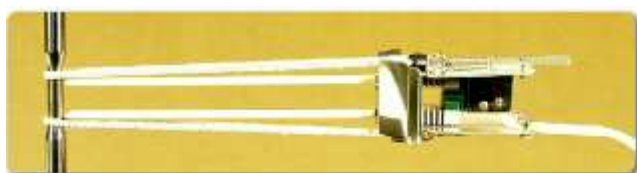


Figure 3. Extensometer made by Epsilontech

The experimental investigation is conducted according to the following procedure:

- 1) The specimen made of steel 1.4859 M is fixed in the testing machine.
- 2) The extensometer is mounted and the heating section is closed.

- 3) Initial working temperature of 100 °C is adjusted.
- 4) The measuring device is put to zero and the heating section is switched on.
- 5) After reaching the required temperature the heating section is left to work at least 1 hour [7]. Then the elongation is measured with the extensometer.
- 6) Steps 3 and 5 are repeated for temperatures of 200, 300, 400, 500, 600, 700, 800, 900 and 1000 °C.

Additionally, three specimens are tested at temperature of 20 °C. Processed test results are shown in Table 2.

Table 2. Processed experimental results

$T_i$ [°C]	$\Delta L_1^{T_i}$ [μm]	$\Delta L_2^{T_i}$ [μm]	$\Delta L_3^{T_i}$ [μm]	$\Delta L_{cp}^{T_i}$ [μm]	$\alpha^{T_i}$ [m/m.°C]
$T_1 = 100$	46	59	51	52	$26.00 \times 10^{-6}$
$T_2 = 100$	105	117	111	111	$24.67 \times 10^{-6}$
$T_3 = 300$	160	175	166	167	$23.86 \times 10^{-6}$
$T_4 = 400$	212	225	223	220	$23.16 \times 10^{-6}$
$T_5 = 500$	267	276	273	272	$22.67 \times 10^{-6}$
$T_6 = 600$	319	328	322	323	$22.28 \times 10^{-6}$
$T_7 = 700$	369	377	373	373	$21.94 \times 10^{-6}$
$T_8 = 800$	421	426	425	424	$21.74 \times 10^{-6}$
$T_9 = 900$	472	475	475	474	$21.54 \times 10^{-6}$
$T_{10} = 1000$	525	525	528	526	$21.47 \times 10^{-6}$

Figure 4 shows the graphic representation of the relationship between expansion coefficient and the temperature. The elongation measured with the extensometer of specimens 1, 2 and 3 is denoted

with  $\Delta L_1^{T_i}$ ,  $\Delta L_2^{T_i}$ ,  $\Delta L_3^{T_i}$  respectively and the average elongation of the three specimens is denoted by  $\Delta L_{cp}^{T_i}$ .

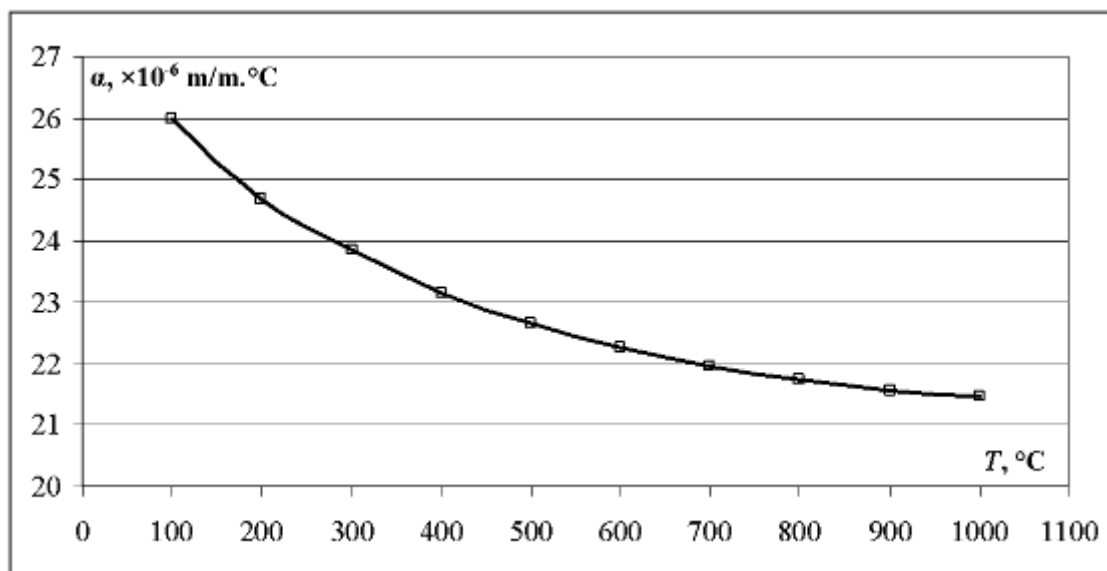


Figure 4. Graphic representation of the relationship between expansion coefficient and the temperature

The thermal expansion coefficient  $\alpha$  is calculated according to the following formula:

$$\alpha^{T_i} = \frac{\Delta L_{cp}^{T_i}}{0.025 \cdot (T_i - 20)}$$

The obtained results show that the thermal expansion coefficient of steel type 1.4852 M decreases with the increase of the temperature. After 800 °C its value trends asymptotically to  $21.4 \times 10^{-6}$  m/m°C. This leads to the conclusion that  $\alpha = \text{const} = 21.4 \times 10^{-6}$  m/m°C at temperatures higher than 1000 °C.

#### 4. Conclusion

The thermal expansion coefficient of a new steel type (1.4852 M) is obtained. It is observed that this coefficient decreases with the increase of the temperature. The acquired results can be used for the numerical simulation of the residual stresses and strains in moulds made of 1.4852 M steel.

#### References

1. Nikolov, N. (2009) *Peculiarities in the calculation of residual stresses and deformations in cast beam rear axle of a lorry*. Proceedings of "BulTrans-2009" (First Scientific conference in aviation, automotive and railway equipment and technology) Sozopol, Bulgaria, 24-26 September 2009, p. 149-152
2. Lazov, L., Slavov, I. (1992) *Съпротивление на материалите (Strength of materials)*. Tehnika, Sofia, 1992 (in Bulgarian)

3. Nikolov, N. (2009) *Analysis of residual stress in steel casting and choice of treatment for their reduction*. Proceedings of "AMO 2009" (The IX International Scientific Conference on Advanced Materials and Processes; Kranevo, Bulgaria, 25-27 June 2009), vol. 1, p. 87-90
4. Tsonev, V. (2011) *Изследване на механичните свойства на легирани стомани при високи температури (Investigation of mechanical properties of alloy steels at high temperatures)*. Ph.D. thesis, Technical University of Sofia, 2011 (in Bulgarian)
5. BS EN 10002-5:1992, *Tensile testing of metallic materials. Method of test at elevated temperatures*. BSI, ISBN 0 580 20403 0  
(see carefully "BS EN ISO 6892-2:2011, *Metallic materials. Tensile testing. Method of test at elevated temperature*")
6. BS EN ISO 9513:2002, *Metallic materials. Calibration of extensometers used in uniaxial testing*. BSI, ISBN 0 580 40511 7  
(see carefully "BS EN ISO 9513:2012, *Metallic materials. Calibration of extensometer systems used in uniaxial testing*. BSI, ISBN 978 0 580 83326 7")
7. EN 10291:2000, *Metallic materials. Uniaxial creep testing in tension. Methods of test*. BSI, ISBN 0 580 36703 7

Received in January 2014  
(and revised form in February 2014)